



# Simulieren of experimenteren?

Wim Platschorre

8 juni 2018

2

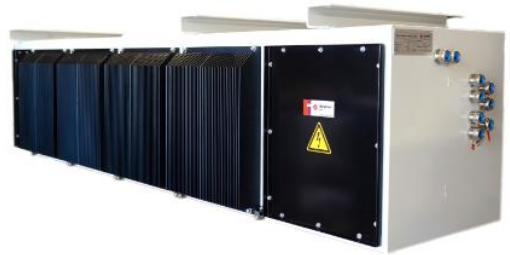
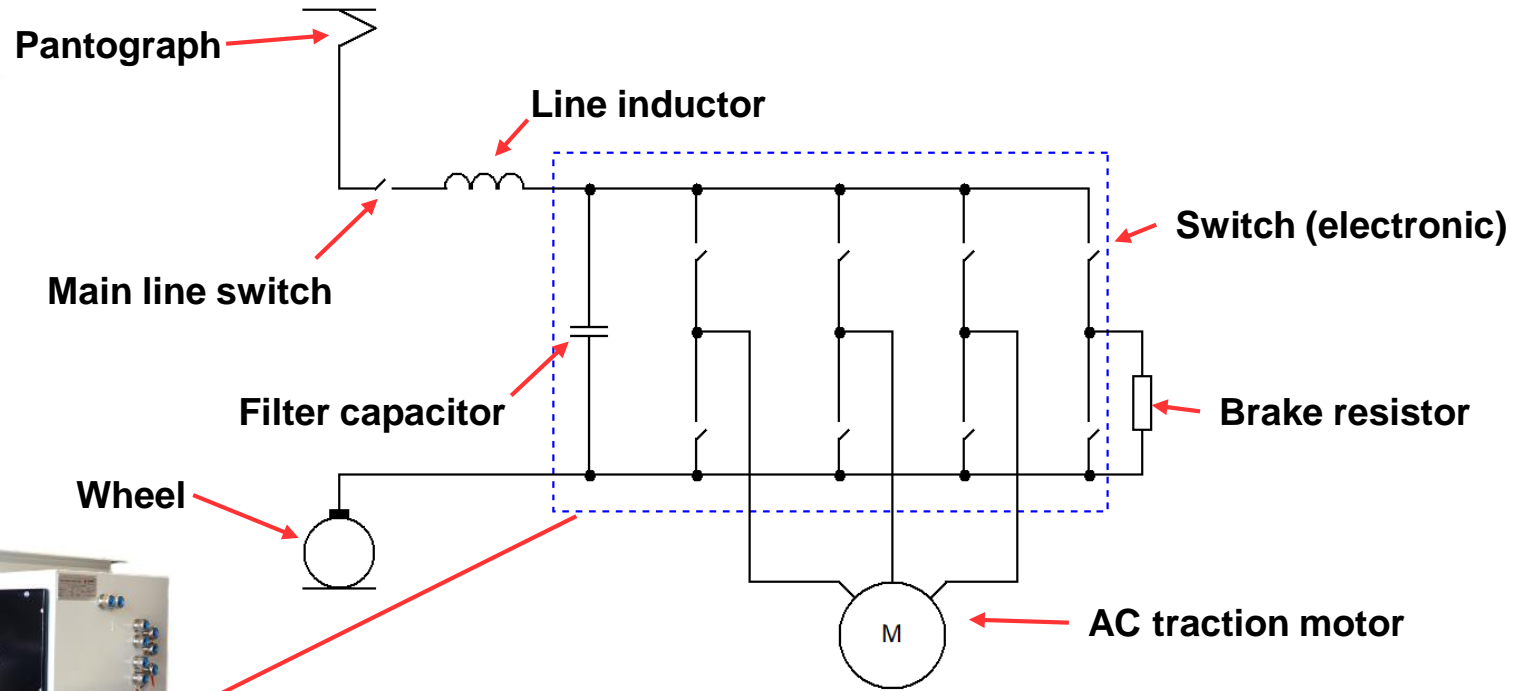
14 juni 2018  
1931 Congressentrum Den Bosch

**POWER  
ELECTRONICS**

**2018**

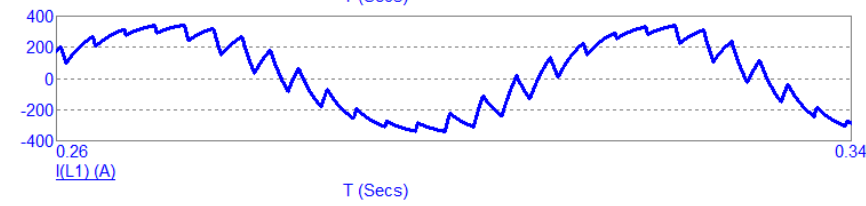
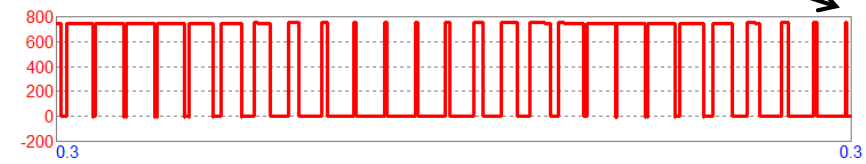
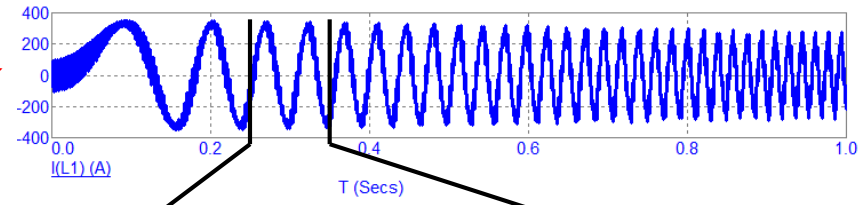
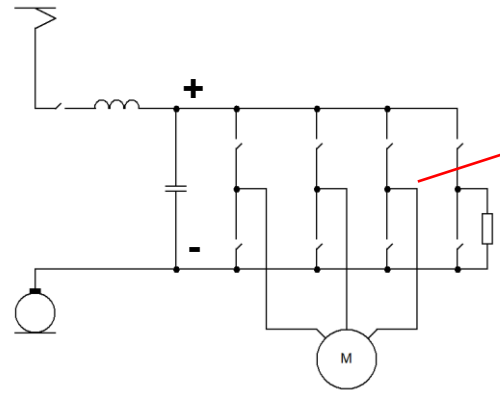


# Basic traction drive circuit





# DC-AC converter: inverter + brake chopper



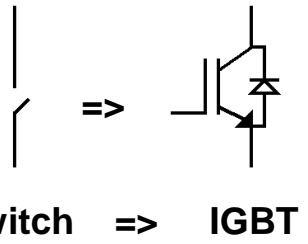
$V_{CE} = 4500\text{ V}$   
 $I_c = 1200\text{ A}$

**ABB HiPak™**

**IGBT Module**  
**5SNA 1200G450300**

Doc. No. 5SVA 1401-03 04-2012

- Ultra low-loss, rugged SPT™ chip-set
- Smooth switching SPT™ chip-set for good EMC
- Industry standard package
- High power density
- AISiC base-plate for high power cycling capability
- AlN substrate for low thermal resistance

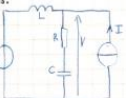


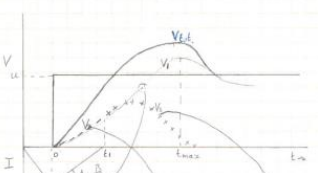
# 30 jaar geleden: handwerk

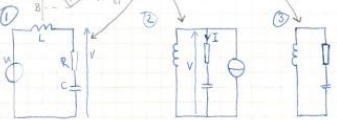
**HOLEC M4**  
holtec machines & apparaten bv

**BEREKENINGSFORMULIER**

offerteopdracht nr.: \_\_\_\_\_ datum: BZ1024  
 project: \_\_\_\_\_ aantal bladen: \_\_\_\_\_ bl.  
 onderwerp: dw/elt, overzet bij 2rukba. behandeld: PSE  
 gecontroleerd: \_\_\_\_\_

gegevens:  
  
 $I = \text{commutatorstroom}$   
 $R, C = \text{snubber}$   
 $U = \text{commutatorspanning, bij openen v.d. diode}$   
 $I = \text{recovery stream diode}$   
 $\beta = \frac{R}{\omega L} \quad \omega = \sqrt{\frac{1}{LC} - \omega^2}$






①  $t_{max} = \arctan\left(\frac{-\beta}{\omega - \beta^2/\omega}\right) + \pi$   
 $V(t) = U(1 + e^{-\beta t}) \cdot (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t)$   
 ②  $V(t_1) = A \cdot L(1 + e^{-\beta t_1}) \cdot (\frac{\omega}{\omega_0} \sin \omega t_1 - \cos \omega t_1)$   
 $I_2(t) = \frac{A}{\omega} e^{-\beta t} \cdot \sin \omega t$   
 ③  $V_2(t) = V(t) \cdot e^{-\beta(t-t_1)} \cdot \cos \omega(t-t_1) + \frac{I_2(t_1)}{\omega} \cdot \frac{-\beta V_2(t_1)}{\omega} \cdot e^{-\beta(t-t_1)} \cdot \sin \omega(t-t_1)$   
 $V_{tot} = V_2(t) + V_1(t)$  (tot. bijdrage  $t_1$ )  
 $V_{tot} = V_2(t) + V_1(t)$  (norm. bijdrage  $t_1$ )

**HOLEC M4**  
holtec machines & apparaten bv

**BEREKENINGSFORMULIER**

offerteopdracht nr.: \_\_\_\_\_ datum: \_\_\_\_\_  
 project: \_\_\_\_\_ aantal bladen: \_\_\_\_\_ bl.  
 onderwerp: \_\_\_\_\_ behandeld: \_\_\_\_\_  
 gecontroleerd: \_\_\_\_\_

evens:  
  
 $I_1 = \frac{U}{R}$   
 $I_2 = \frac{U}{\omega L}$   
 $I = I_1 + I_2$   
 $V = U - I \cdot R = U - (I_1 + I_2) \cdot R = U - I_1 R - I_2 R = U - U - \frac{U R}{\omega L} = -\frac{U R}{\omega L}$   
 $\beta = \frac{R}{\omega L} \quad \omega = \sqrt{\frac{1}{LC} - \omega^2}$

**HOLEC M4**  
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**BEREKENINGSFORMULIER**

offerteopdracht nr.: \_\_\_\_\_ datum: BZ1012  
 project: \_\_\_\_\_ aantal bladen: \_\_\_\_\_ bl.  
 onderwerp: \_\_\_\_\_ behandeld: PSE  
 gecontroleerd: \_\_\_\_\_

gegevens:  
 $V = U(1 + e^{-\beta t})(\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (B \cos \omega t + C \sin \omega t)$   
 $\frac{dV}{dt} = -\beta U e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t) - \beta U_0 e^{-\beta t} (B \cos \omega t + C \sin \omega t)$   
 $\frac{dV}{dt} = -\beta U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 $\frac{dV}{dt} = U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 $\frac{dV}{dt} = U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 maximale  $\frac{dV}{dt}$ :  $\frac{dV}{dt} = 0 \Rightarrow (\omega - \beta) \sin \omega t + \beta \cos \omega t = 0$   
 $\tan \omega t = \frac{\beta}{\omega - \beta}$   
 $t = \arctan\left(\frac{\beta}{\omega - \beta}\right) + \pi$   
 $t$  invullen in ③

**HOLEC M4**  
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**BEREKENINGSFORMULIER**

offerteopdracht nr.: \_\_\_\_\_ datum: SZ1013  
 project: \_\_\_\_\_ aantal bladen: \_\_\_\_\_ bl.  
 onderwerp: dw/elt behandeld: PSE  
 gecontroleerd: \_\_\_\_\_

gegevens:  
 $V = U(1 + e^{-\beta t})(\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (B \cos \omega t + C \sin \omega t)$   
 $\frac{dV}{dt} = -\beta U e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t) - \beta U_0 e^{-\beta t} (B \cos \omega t + C \sin \omega t)$   
 $\frac{dV}{dt} = -\beta U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 $\frac{dV}{dt} = U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 $\frac{dV}{dt} = U_0 e^{-\beta t} (\frac{\omega}{\omega_0} \sin \omega t - \cos \omega t) + U_0 e^{-\beta t} (\omega B \cos \omega t - \omega C \sin \omega t - \beta B \cos \omega t - \beta C \sin \omega t)$   
 maximale  $\frac{dV}{dt}$ :  $\frac{dV}{dt} = 0 \Rightarrow (\omega - \beta) \sin \omega t + \beta \cos \omega t = 0$   
 $\tan \omega t = \frac{\beta}{\omega - \beta}$   
 $t = \arctan\left(\frac{\beta}{\omega - \beta}\right) + \pi$   
 $t$  invullen in ③

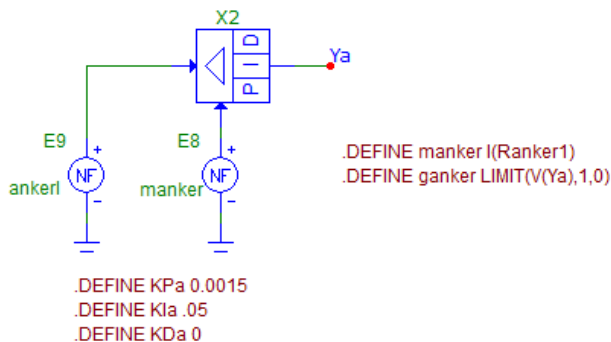
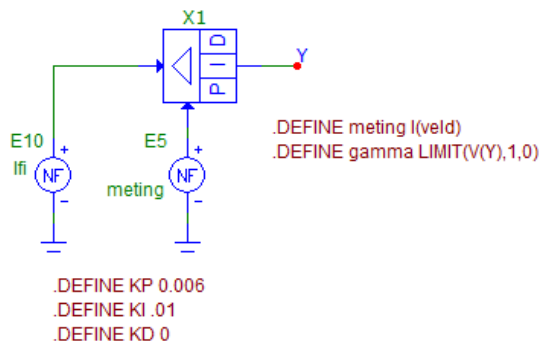
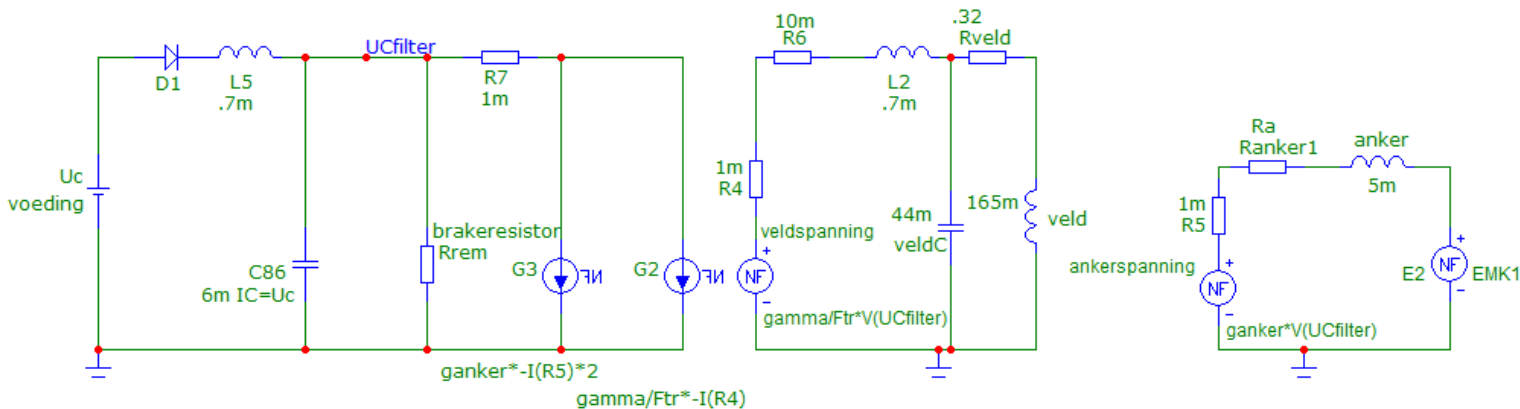
## Waarom simuleren?

Onmogelijk om elk parasitair effect te berekenen. Beperkingen afhankelijk van het doel en de te simuleren tijdsduur.

Daarom 3 niveaus voor (elektrische) simulatie:

doel	model
Regelgedrag	Lineair omzettermodel
Circuitgedrag	Eenvoudig, snel schakelaarmodel, diode met reverse recovery
Halfgeleidergedrag t.b.v. driverontwerp	Gedragmodel of fysisch model

# Lineair omzettermodel: chopper voor DC-motor



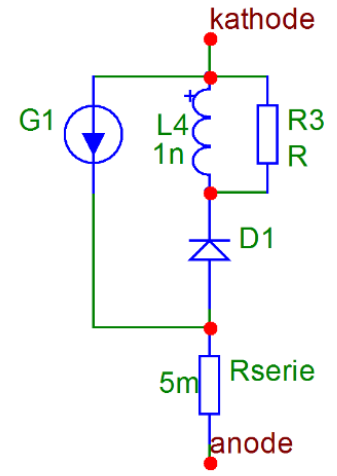
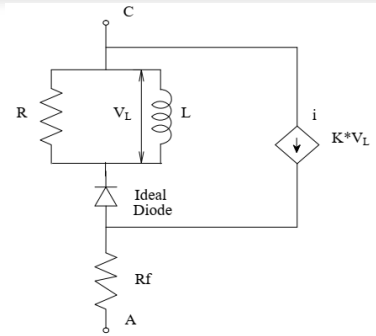
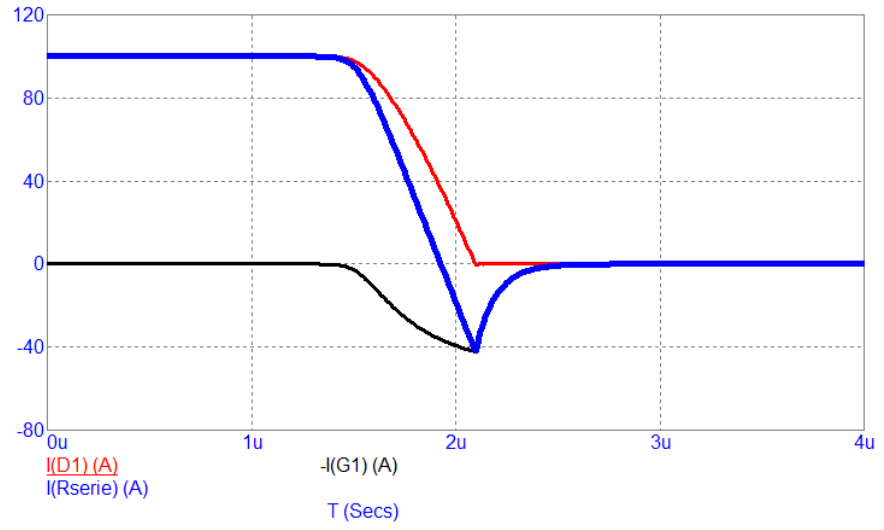


# Gedragmodel: diode reverse recovery

Proceedings of the 7th WSEAS International Conference on Power Systems, Beijing, China, September 15-17, 2007 48

## A New Macro-Model for Power Diodes Reverse Recovery

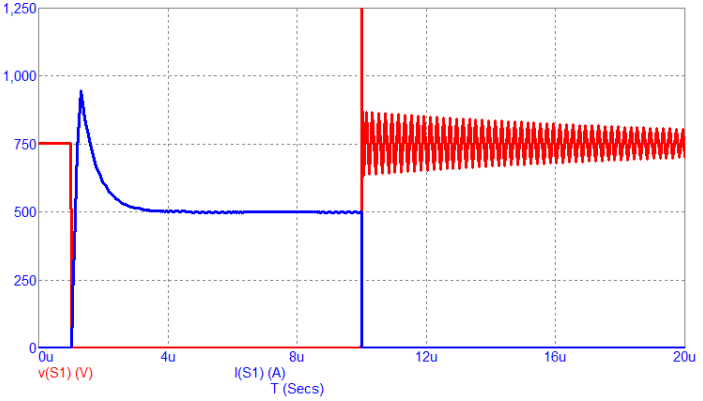
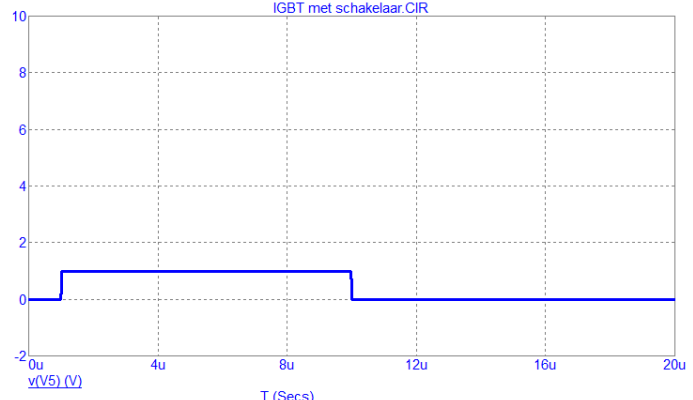
ALI DASTFAN  
Department of Electrical & Robotic Engineering  
Shahrood University of Technology  
Shahrood, Iran



.parameters (K,R)

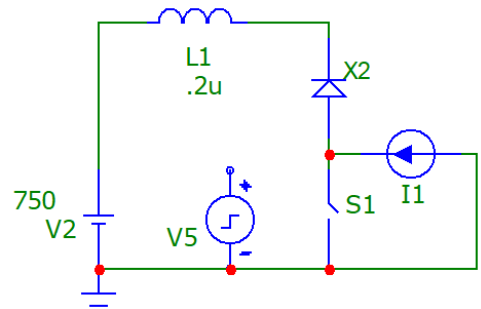


# Standaard schakelaar



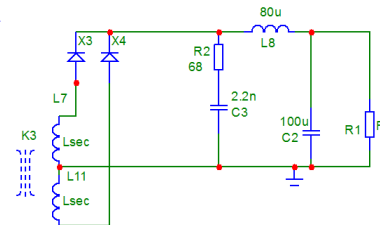
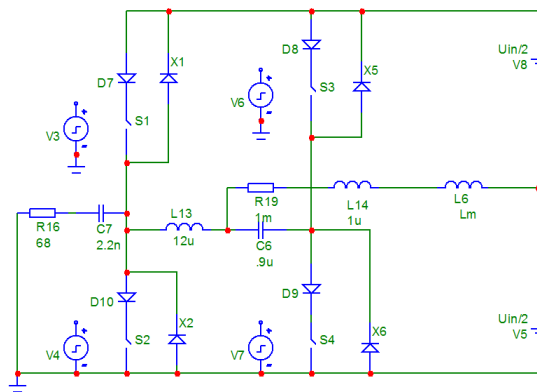
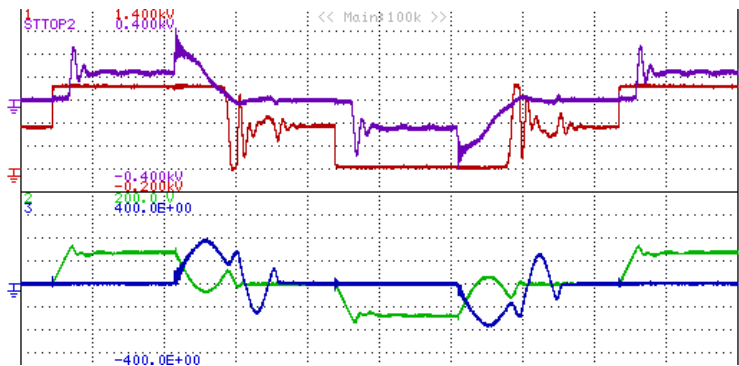
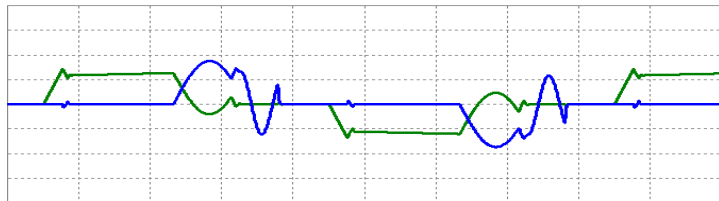
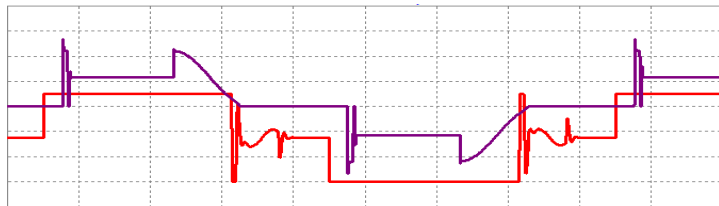
Oscillaties vertragen de simulatie: snubber nodig

```
.DEFINE K 600  
.DEFINE R 0.002  
.DEFINE current 500
```

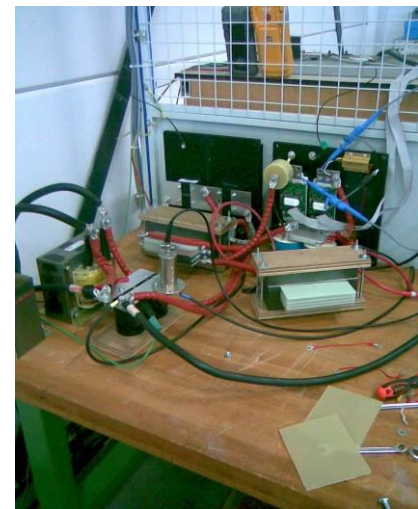




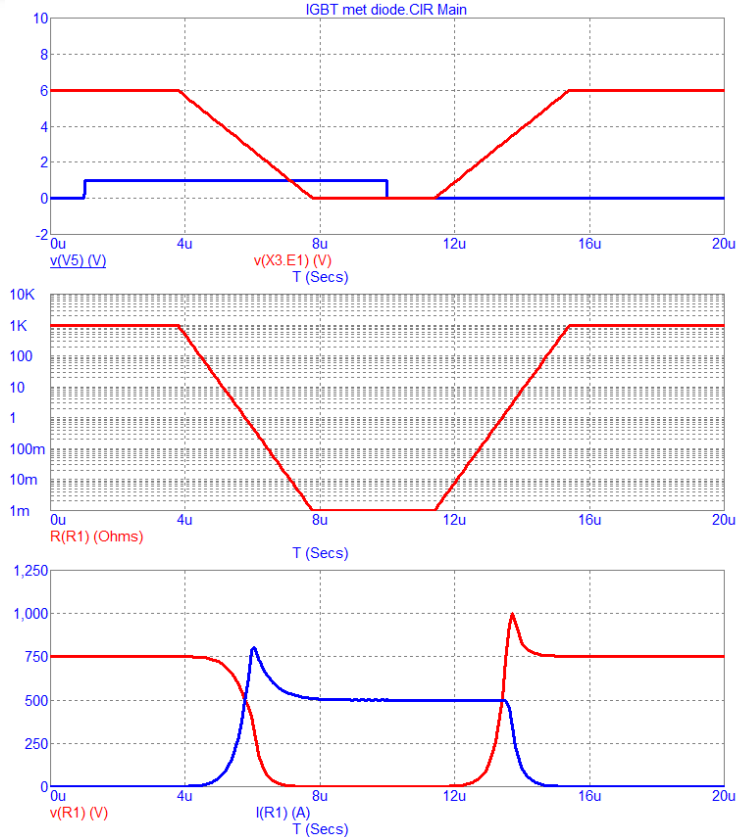
# Voorbeeld: HF dc-dc omzetter



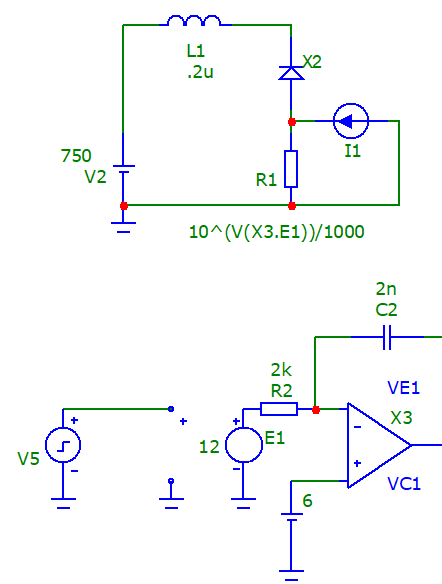
- 8: secundaire fasespanning [100V/div]
- 1: primaire fasespanning [200V/div]
- 2: primaire fasestroom [50A/div]
- 3: resonante stroom [50A/div]



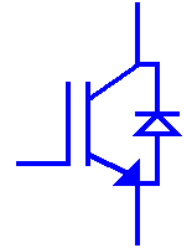
# Met variabele weerstand: veel beter



```
.DEFINE K 600  
.DEFINE R 0.002  
.DEFINE current 500
```

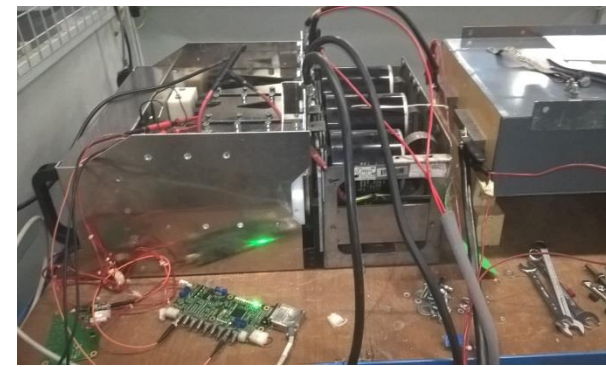
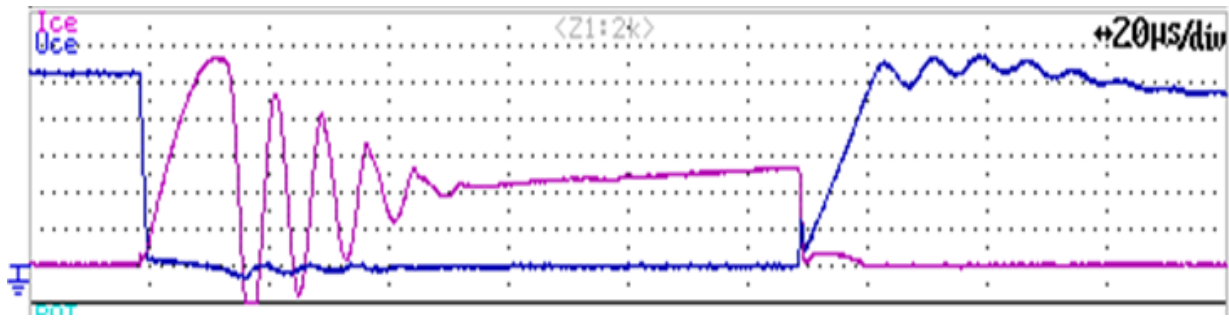
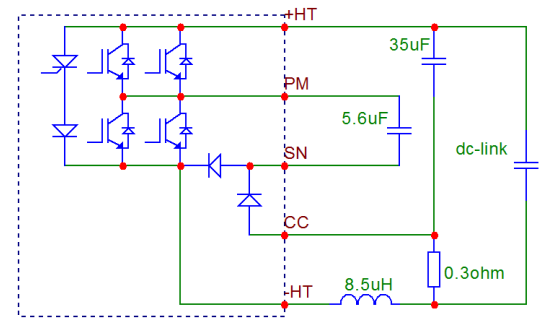
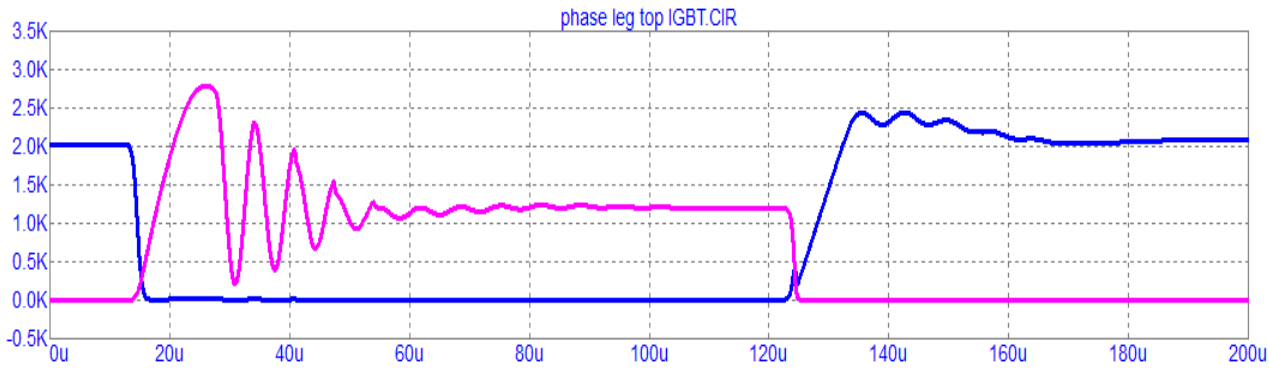


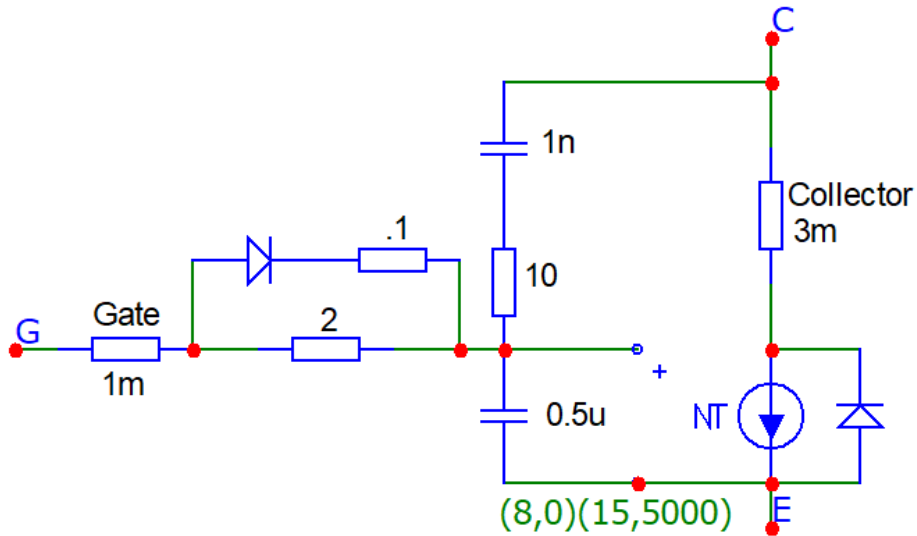
$R = 10^V/1000$   
met  $V=6V$ :  $R=10^6/1000=1k\Omega$   
met  $V=0V$ :  $R=10^0/1000=1m\Omega$



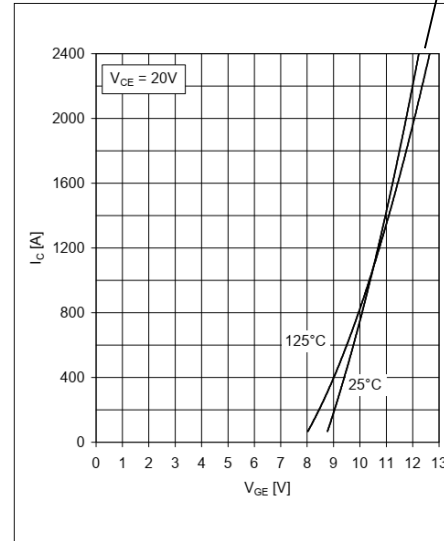


# Voorbeeld: gesnubberde IGBT





5000A



15V

Fig. 2 Typical transfer characteristics, chip level

Table 2.1: Micro-Cap 9 IGBT Modeling Parameters

Parameter	Description	Units
AGD	Gate-drain overlap area	m <sup>2</sup>
BVN	Avalanche multiplication exponent	
JSNE	Emitter saturation current density	A/cm <sup>2</sup>
MUN	Electron mobility	cm <sup>2</sup> /(V·s)
VT	Threshold area	V
AREA	Device area	m <sup>2</sup>
CGS	Gate-source capacitance per unit area	F/cm <sup>2</sup>
KF	Triode region factor	
MUP	Hole mobility	cm <sup>2</sup> /(V·s)
TAU	Ambipolar recombination lifetime	s
VTD	Gate-drain overlap depletion threshold	V
BVF	Avalanche uniformity factor	
COXD	Gate-drain oxide capacitance per unit area	F/cm <sup>2</sup>
KP	MOS transconductance	A/V <sup>2</sup>
NB	Base doping	cm <sup>-3</sup>
THETA	Transverse field factor	V <sup>-1</sup>
WB	Metallurgical base width	m

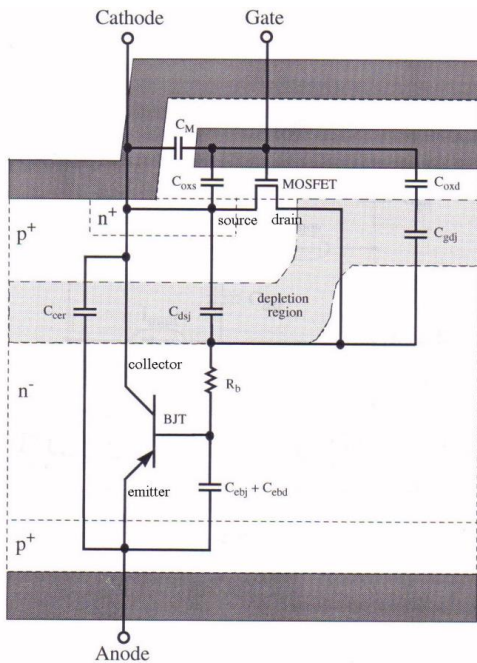


Figure 2.2: Phenomenological IGBT equivalent circuit [44].

Source: Local page 'Models'

AGD	7m	AREA	7m	BVF	1
BVN	10	CGS	1	COXD	1
JSNE	20p	KF	1	KP	1200
MUN	20k	MUP	400	NB	20T
T_ABS	undefined	T_MEASURED	undefined	T_REL_GLOBAL	undefined
T_REL_LOCAL	undefined	TAU	1	THETA	10
VT	10	VTD	0	WB	80u

**Parameters moeilijk te verkrijgen  
=> eindeloos uitproberen**

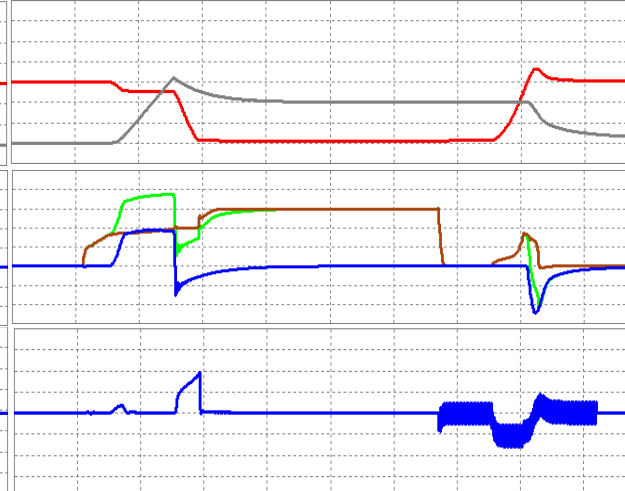
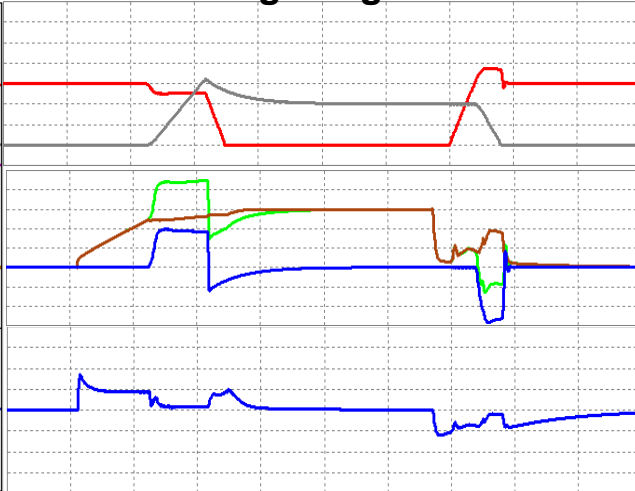
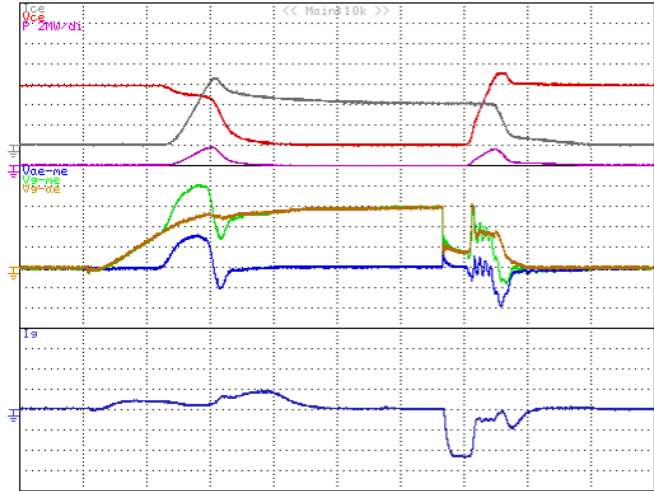


# Experiment en simulatie

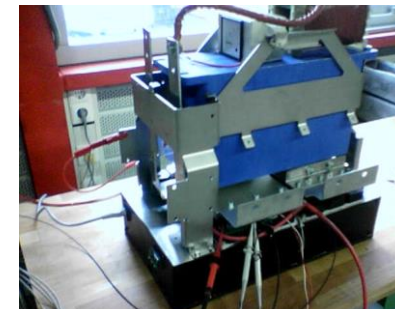
Meting: 1kA @1,5kV in en uit

1µs/div Simulatie met gedragsmodel

Simulatie met fysisch model



CH1	CH2	CH3	CH4	CH7
0.500kV	0.500kV	5.00 V	5.00 V	5.00 V
DC1MΩ	DC1MΩ	DC1MΩ	DC1MΩ	AC1MΩ
Math1 C4-C3		Math2 C1*C2		





# Nieuwe generatie IGBT's

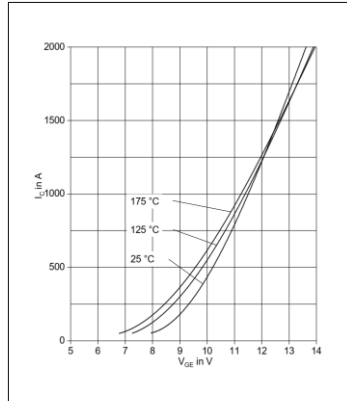
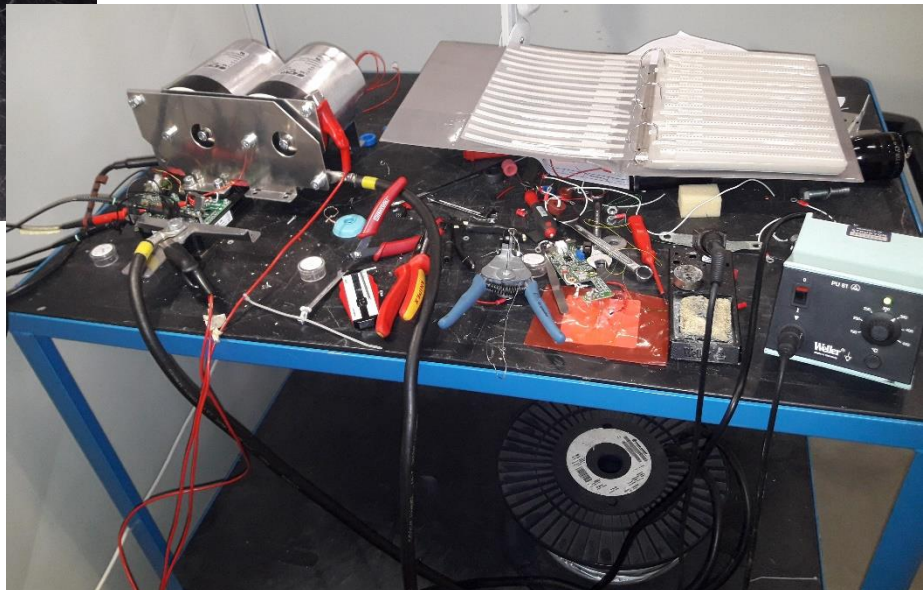
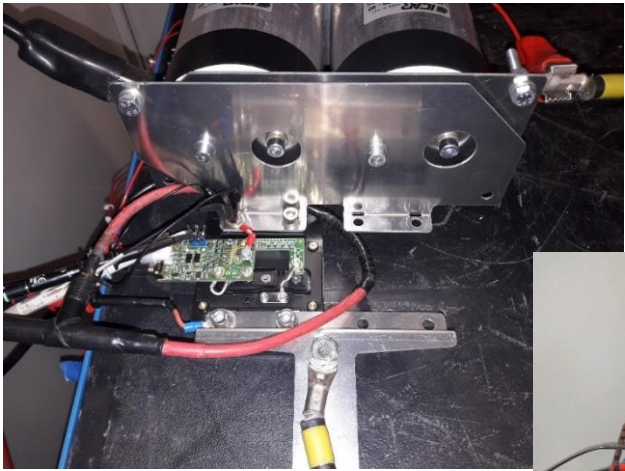
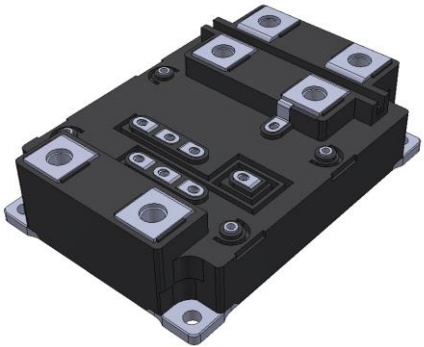
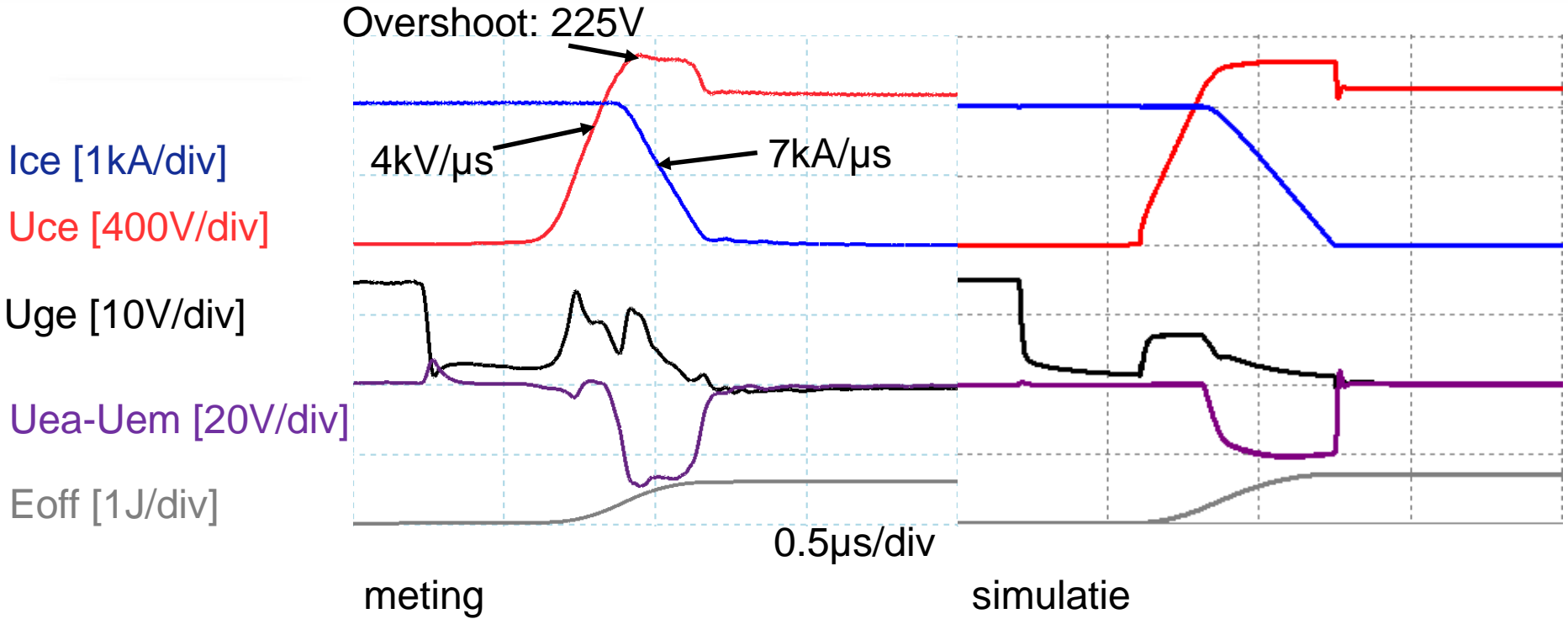


Fig. 2 Typical transfer characteristics, chip level

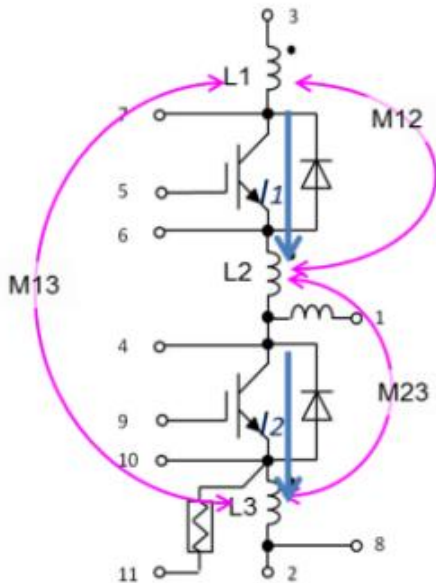


# Resultaat 2000A uitschakelen

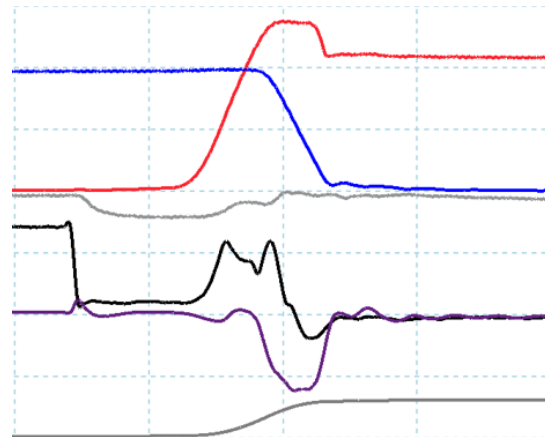
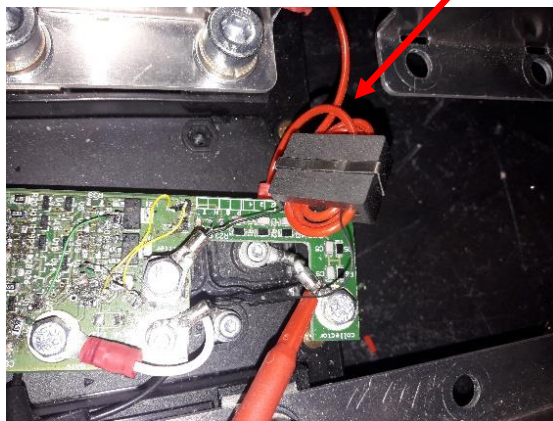




# Trafo: niet simuleren, alleen experimenteren



**Probleem:  $L2 \approx 0$**   
**Oplossing:  $U(L1)$  transformeren naar emitterniveau**



High side



**Strukton**  
Rail

14 juni 2018  
1931 Congrescentrum Den Bosch

**POWER**  
**ELECTRONICS**

2018

# Vragen?

wim.platschorre@strukton.com